

FIG. 3. Schematic representation of multiple exposure technique.

curately determined from measurements of the parameters of the corresponding ellipse.

It was found that the measurements of the film and specimen distance from the x-ray source constitute the principal source of error. These distances are shown in Fig. 1 as a and b, respectively. To eliminate this and other error sources, a number of innovations in experimental and measuring techniques were introduced which will be described presently.

It may be seen from Fig. 1 that the following direct relationship can be established between  $\alpha$ ,  $\beta$  and the slopes  $m_1$ ,  $m_2$  of the diffracted rays:

$$m_1 = p/c = \tan(\alpha + \beta), \tag{1}$$

$$m_2 = q/c = \tan(\alpha - \beta), \qquad (2)$$

where  $\alpha$  is the semiapex angle of the incident x-ray cone equal to  $\pi/2-\theta$ ,  $\theta$  being the Bragg angle, and  $\beta$  is the angle subtended by the normal of the reflecting (*hkl*) plane and the axis of the x-ray tube.  $c=x_1-x_2$  is the distance between two consecutive film positions (Fig. 3).

If the slope parameters  $m_1$  and  $m_2$  of an (hkl) reflection are experimentally determined, one obtains the value of  $\alpha$  and therefore the corresponding value of the Bragg angle  $\theta$  from the solution of Eqs. (1) and (2). Subsequent substitution in the Bragg equation yields the corresponding d value.

The determination of the d spacing of an (hkl) set of planes is thus independent of the troublesome a and bparameters if the slopes  $m_1$  and  $m_2$  of the diffracted rays can be obtained. The principal innovation consists, therefore, of a precision determination of the slopes by a method of least squares employing a multiple exposure technique and exact measurements of distances between consecutive film positions. This is accomplished through the use of precision spacers. Thus in this method the film, after being exposed once, is moved a known distance  $(x_1 - x_2)$  and a second exposure is taken. After repeating this procedure seven or eight times the film is processed in the usual way. Consequently, instead of a single ellipse, one obtains a pattern consisting of a family of seven or eight ellipses corresponding to one (hkl) reflection. Figure 2 represents such a multiple exposure diagram of an undeformed, zone-refined tungsten crystal in which the elliptical patterns have been recorded at eight different film positions  $(x_1 \text{ to } x_8)$ .

Figure 3 shows schematically the multiple exposure method. The points  $y_8$  and  $y_7$  are the intersections of the major axis with the ellipse produced during the first exposure and  $x_7$  is the distance of the film from a fixed origin 0. Similarly,  $y_9$  and  $y_6$  are the intersections with the second ellipse and  $x_6$  is the corresponding film distance, and so on.

If the equation to the line  $y_1y_7$  is

 $y = m_1 x + B_1,$ 

one obtains by means of the least-squares method (see Appendix A)

$$m_1 = \sum y_i(x_i - \bar{x}) / \sum (x_i - \bar{x})^2, \quad i = 1, 2, 3 \cdots 7.$$

But the slope of this line is also  $\tan(\alpha + \beta)$ , and

$$Km_1 = \tan(\alpha + \beta), \tag{3}$$

where K is the film shrinkage factor. Similarly for the line  $y_{14}y_8$ ,

$$Km_2 = \tan(\alpha - \beta). \tag{4}$$

By combining Eqs. (3) and (4),

$$\alpha = \frac{1}{2} \left[ \arctan(Km_1) + \arctan(Km_2) \right].$$
(5)

Also  $\theta = \pi/2 - \alpha$ . Therefore

$$d = \lambda/2 \cos \alpha.$$
 (6)

## 3. EXPERIMENTAL TECHNIQUE

The precision measurements of the d spacings and lattice parameters by the divergent beam method depend on a number of factors which must be closely controlled and which will be presently discussed.

## a. Film Measurements

It has been shown that the precision of the d values is greatly dependent on the accuracy of the slope parameters  $m_1$  and  $m_2$ , which in turn depend on the accuracy of measurements of the  $y_n$  ordinates and  $x_n$  abscissas of the multiple exposure diagram (Fig. 3).

The  $y_n$  coordinates are measured along the major axis of the ellipse corresponding to a specific (*hkl*) reflection, this axis being extended through the entire family of ellipses generated by the multiple exposure technique. Before the major axis can be constructed it is necessary to determine the center of the film. If the points of intersection of two families of ellipses  $p_1$ ,  $p_2$ etc. are connected, a line is produced which extrapolates through the center of the film (Fig. 2). If this process is repeated for a number of intersections, it is possible to locate this center accurately. Once it has been located, a major axis is constructed on the film with the aid of precision dividers. The actual readings of the  $y_2$  coordinates recording mi line profiles out along th of the profile fine the end-

The  $x_n$  co

spacers which which span t 95 mm down which can be the film and fore, the sele governed by o of the elliptic portions of th consequently on crystal o spacing of pla

To insure a nates it is nec film should be main placement. If machining groups of that a vacuing that a vacuing that a vacuing the second sec

It was obser the *d* spacings increasing  $\theta$  vato record a greof the center of the diffracter tube itself, a 1 This tip may b semiapex angle (1/16-in.) dian

## b.

A number of have to be take It is, for examshrinkage be u d spacings betw form are to be u analysis After DuPont Crona  $(10 \times 12 \text{ in.})$  sat shrinkage. Corimpressing a st measuring it aft